

# The Euler system on a space curve

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# The Euler system

Consider flows of an inviscid medium

$$\begin{cases} \rho(u_t + uu_a) = -p_a - \rho gh', \\ \rho_t + (\rho u)_a = 0, \\ \rho T (s_t + us_a) - kT_{aa} = 0, \end{cases} \quad (1)$$

on a naturally-parametrised space curve in the three-dimensional Euclidean space

$$M = \{x = f(a), y = g(a), z = h(a)\}.$$

in a field of constant gravitational force.

# Thermodynamics

A thermodynamic state is a two-dimensional Legendrian manifold  $L \subset \mathbb{R}^5(p, \rho, s, T, \epsilon)$ , a maximal integral manifold of the differential 1-form

$$\theta = d\epsilon - Tds - p\rho^{-2}d\rho,$$

i.e. a manifold such that the first law of thermodynamics  $\theta|_L = 0$  holds.

Following [1], we require that the quadratic differential form

$$\kappa = d(T^{-1}) \cdot d\epsilon - \rho^{-2}d(pT^{-1}) \cdot d\rho$$

on the surface  $L$  be negative definite,

$$\kappa|_L < 0,$$

and the entropy  $s$  satisfies the inequality  $s \leq s_0$ , where the constant  $s_0$  depends on the nature of a process under consideration.

# Thermodynamics

Consider the projection  $\pi: (p, \rho, s, T, \epsilon) \mapsto (p, \rho, s, T)$ . The restriction of this map on the state surface  $L$  is a diffeomorphism  $\bar{L} = \pi(L)$ , and the surface  $\bar{L} \subset \mathbb{R}^4$  is a Lagrangian manifold in the 4-dimensional symplectic space  $\mathbb{R}^4$  equipped with the structure form

$$\Omega = d\theta = ds \wedge dT + \rho^{-2} d\rho \wedge dp.$$

Thus, the *thermodynamic state* is the Lagrangian submanifold  $\bar{L}$  in the symplectic space  $(\mathbb{R}^4, \Omega)$ :

$$\begin{cases} f(p, \rho, s, T) = 0, \\ g(p, \rho, s, T) = 0, \end{cases} \quad \text{and} \quad [f, g]|_{\bar{L}} = 0, \quad (2)$$

where  $[f, g]$  is the Poisson bracket, and the symmetric differential form  $\kappa$  is negative definite on this surface.

# Symmetry Lie algebra

We consider a Lie algebra  $\mathfrak{g}$  of point symmetries of the Euler system (1).

Let  $\vartheta: \mathfrak{g} \rightarrow \mathfrak{h}$  be the following Lie algebras homomorphism

$$\vartheta: X \mapsto X(\rho)\partial_\rho + X(s)\partial_s + X(p)\partial_p + X(T)\partial_T,$$

where  $\mathfrak{h}$  is a Lie algebra generated by vector fields that act on the thermodynamic variables  $p$ ,  $\rho$ ,  $s$  and  $T$ .

The kernel of the homomorphism  $\vartheta$  is an ideal  $\mathfrak{g}_m \subset \mathfrak{g}$  (geometric symmetries).

Let also  $\mathfrak{h}_t$  be the Lie subalgebra of the algebra  $\mathfrak{h}$  that preserves thermodynamic state (2).

## Theorem

*A Lie algebra  $\mathfrak{g}_{\text{sym}}$  of symmetries of the Euler system  $\mathcal{E}$  coincides with*

$$\vartheta^{-1}(\mathfrak{h}_t).$$

# Symmetry Lie algebra

Let  $h(a)$  be an arbitrary function.

The Lie algebra  $\mathfrak{g}$  of point symmetries of the system (1) is generated by the vector fields

$$\begin{aligned}X_1 &= \partial_t, & X_4 &= T \partial_T, \\X_2 &= \partial_p, & X_5 &= p \partial_p + \rho \partial_\rho - s \partial_s. \\X_3 &= \partial_s,\end{aligned}$$

The pure thermodynamic part  $\mathfrak{h}$  of the system symmetry algebra is

$$\begin{aligned}Y_1 &= \partial_p, & Y_3 &= T \partial_T, \\Y_2 &= \partial_s, & Y_4 &= p \partial_p + \rho \partial_\rho - s \partial_s.\end{aligned}$$

Thus, in this case the system of differential equations  $\mathcal{E}$  has the smallest Lie algebra of point symmetries  $\vartheta^{-1}(\mathfrak{h}_t)$ .

# Symmetry Lie algebra

- $h(a)$  is arbitrary

$$\begin{aligned}X_1 &= \partial_t, & X_2 &= \partial_\rho, & X_3 &= \partial_s, & X_4 &= T \partial_T, \\X_5 &= \rho \partial_\rho + \rho \partial_\rho - s \partial_s\end{aligned}$$

- $h(a) = \text{const}$

$$\begin{aligned}X_6 &= \partial_a, & X_7 &= t \partial_a + \partial_u, \\X_8 &= t \partial_t + a \partial_a - s \partial_s, \\X_9 &= t \partial_t - u \partial_u - 2\rho \partial_\rho + s \partial_s,\end{aligned}$$

- $h(a) = \lambda a, \lambda \neq 0$

$$\begin{aligned}X_6 &= \partial_a, & X_7 &= t \partial_a + \partial_u, \\X_8 &= t \partial_t + 2a \partial_a + u \partial_u - 2\rho \partial_\rho - s \partial_s, \\X_9 &= \left(\frac{t^2}{2} + \frac{a}{\lambda g}\right) \partial_a + 2\left(t + \frac{u}{\lambda g}\right) \partial_u - \frac{2\rho}{\lambda g} \partial_\rho\end{aligned}$$

- $h(a) = \lambda a^2, \lambda \neq 0$

$$\begin{aligned}X_6 &= a \partial_a + u \partial_u - 2\rho \partial_\rho, \\X_7 &= \sin(\sqrt{2\lambda g} t) \partial_a + \sqrt{2\lambda g} \cos(\sqrt{2\lambda g} t) \partial_u, \\X_8 &= \cos(\sqrt{2\lambda g} t) \partial_a - \sqrt{2\lambda g} \sin(\sqrt{2\lambda g} t) \partial_u\end{aligned}$$

# Symmetry Lie algebra

- $h(a) = \lambda_1 a^{\lambda_2}$ ,  $\lambda_2 \neq 0, 1, 2$   
 $X_6 = t \partial_t - \frac{2a}{\lambda_2 - 2} \partial_a - \frac{\lambda_2 u}{\lambda_2 - 2} \partial_u + \frac{2\lambda_2 \rho}{\lambda_2 - 2} \partial_\rho - s \partial_s$
- $h(a) = \lambda_1 e^{\lambda_2 a}$ ,  $\lambda_2 \neq 0$   
 $X_6 = t \partial_t - \frac{2}{\lambda_2} \partial_a - u \partial_u - \rho \partial_\rho + \rho \partial_\rho$
- $h(a) = \ln a$   
 $X_6 = t \partial_t + a \partial_a - s \partial_s$



# Lifting curves from the plane

Let a curve in the space be defined as a pair of a plane curve  $(x(\tau), y(\tau))$  and a 'lifting' function  $z(\tau)$ .

Let  $l(\tau) = \int_0^\tau \sqrt{x_\theta^2 + y_\theta^2} d\theta$  – the length of the plane curve.

Then the following relation between natural parameter  $a$  and the parameter  $\tau$  is valid

$$h_a = \frac{z_\tau}{\sqrt{x_\tau^2 + y_\tau^2 + z_\tau^2}}.$$

## 1. $h(a) = \text{const}$

The first way of lifting a plane curve is to translate the whole curve along  $z$ -axis, i.e. if  $h(a) = \text{const}$  then  $z(\tau) = \text{const}$ .

## Lifting curves from the plane

2.  $h(a) = \lambda a, \lambda \neq 0$

The second way to lift curve is lifting proportional to the length of the plane part, i.e. if  $h(a) = \lambda a$  then we have the following differential equation on the 'lifting' function  $z(\tau)$

$$(1 - \lambda^2) z_\tau^2 = \lambda^2 (x_\tau^2 + y_\tau^2),$$

solving which given  $1 - \lambda^2 > 0$ , we get

$$z(\tau) = \pm \frac{\lambda}{\sqrt{1 - \lambda^2}} l(\tau) + C,$$

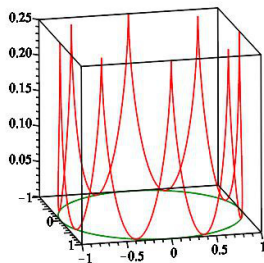
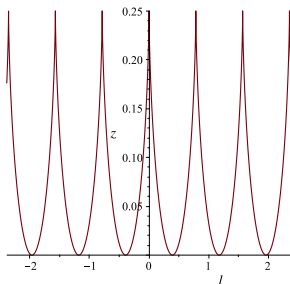
where  $l(\tau)$  – is length of plane projection of curve and  $C = \text{const}$ .  
If  $\lambda = \pm 1$ , then  $x(t) = y(t) = \text{const}$  and we have a vertical line.

# Lifting curves from the plane

3.  $h(a) = \lambda a^2$ ,  $\lambda \neq 0$

The relation between the 'lifting' function  $z(\tau)$  and the length  $l(\tau)$  of the plane curve is

$$\sqrt{4\lambda z(1 - 4\lambda z)} - \arccos(\sqrt{4\lambda z}) = \pm 4\lambda l(\tau).$$

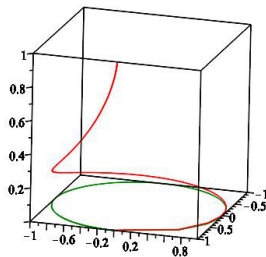
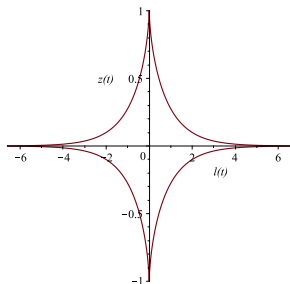


## Lifting curves from the plane

5.  $h(a) = \lambda_1 e^{\lambda_2 a}$

The relation between the 'lifting' function  $z(\tau)$  and the length  $l(\tau)$  of the plane curve is

$$\sqrt{1 - \lambda_2^2 z^2} - \frac{1}{2} \ln \frac{1 + \sqrt{1 - \lambda_2^2 z^2}}{1 - \sqrt{1 - \lambda_2^2 z^2}} = \pm \lambda_2 l(\tau)$$

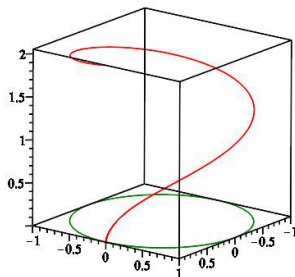
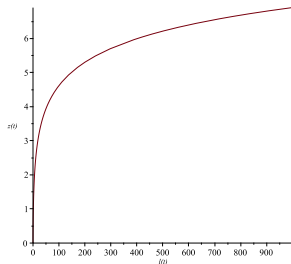


# Lifting curves from the plane

6.  $h(a) = \ln a$

The relation between the 'lifting' function  $z(\tau)$  and the length  $l(\tau)$  of the plane curve is

$$\sqrt{e^{2z} - 1} - \arctan \sqrt{e^{2z} - 1} = \pm l(\tau).$$



# Thermodynamic states

Let  $h(a)$  be an arbitrary function, and let the thermodynamic state admit a one-dimensional symmetry algebra

$$Z = \gamma_1 \partial_p + \gamma_2 \partial_s + \gamma_3 T \partial_T + \gamma_4 (p \partial_p + \rho \partial_\rho - s \partial_s),$$

then the Lagrangian surface  $\bar{L}$  can be found from the conditions  $\{\Omega|_{\bar{L}} = 0, \iota_Z \Omega|_{\bar{L}} = 0\}$ , which lead to the following PDE system on the internal energy

$$\begin{cases} \gamma_4 \rho \epsilon_{\rho\rho} + (\gamma_2 - \gamma_4 s) \epsilon_{\rho s} + \gamma_4 \epsilon_\rho - \gamma_1 \rho^{-2} = 0, \\ (\gamma_2 - \gamma_4 s) \epsilon_{ss} + \gamma_4 \rho \epsilon_{\rho s} - \gamma_3 \epsilon_s = 0. \end{cases}$$

Solving this system for the general case, we have

$$p = C_1 \rho - \frac{\gamma_1}{\gamma_4}, \quad T = C_2 (\gamma_2 - \gamma_4 s)^{-\frac{\gamma_3}{\gamma_4}},$$

where  $C_1, C_2$  are constants. The condition  $\kappa|_L < 0$  leads to the relations

$$\frac{\gamma_3}{\gamma_2 - \gamma_4 s} > 0, \quad C_1 > 0 \quad \text{for all } s \in (-\infty, s_0].$$

# Thermodynamic states

## Theorem

The thermodynamic states admitting a one-dimensional symmetry algebra have the form

$$p = C_1 \rho - \frac{\gamma_1}{\gamma_4}, \quad T = C_2 (\gamma_2 - \gamma_4 s)^{-\frac{\gamma_3}{\gamma_4}},$$

where the constants defining the symmetry algebra satisfy inequalities

$$s_0 < \frac{\gamma_2}{\gamma_4}, \quad C_1 > 0, \quad \frac{\gamma_1}{\gamma_4} < 0,$$

and besides they must meet one of the following conditions:

- 1 if  $\frac{\gamma_3}{\gamma_4}$  is irrational, then  $\gamma_3 > 0$ ,  $\gamma_4 > 0$ ,  $C_2 > 0$ ;
- 2 if  $\frac{\gamma_3}{\gamma_4}$  is rational, then  $\frac{\gamma_3}{\gamma_4} > 0$  (i.e.  $\frac{\gamma_3}{\gamma_4} = \frac{m}{k}$ ) and
  - 1 if  $k$  is even, then  $\gamma_4 > 0$ ,  $C_2 > 0$ ;
  - 2 if  $k$  is odd and  $m$  is even, then  $C_2 > 0$ ;
  - 3 if  $k$  is odd and  $m$  is odd, then  $C_2 \gamma_4 > 0$ .

# Kinematic invariants

We consider two group actions on the Euler system  $\mathcal{E}$  – the prolonged actions of the groups generated by actions of the Lie algebras  $\mathfrak{g}_m$  and  $\mathfrak{g}_{\text{sym}}$ .

A function  $J$  on the manifold  $\mathcal{E}_k$  is a *kinematic differential invariant of order  $\leq k$*  if

- 1  $J$  is a rational function along fibers of the projection  $\pi_{k,0} : \mathcal{E}_k \rightarrow \mathcal{E}_0$ ,
- 2  $J$  is invariant with respect to the prolonged action of the Lie algebra  $\mathfrak{g}_m$ , i.e., for all  $X \in \mathfrak{g}_m$ ,

$$X^{(k)}(J) = 0, \quad (3)$$

where  $\mathcal{E}_k$  is the prolongation of the system  $\mathcal{E}$  to  $k$ -jets, and  $X^{(k)}$  is the  $k$ -th prolongation of a vector field  $X \in \mathfrak{g}_m$ .

A kinematic invariant is an *Euler invariant* if condition (3) holds for all  $X \in \mathfrak{g}_{\text{sym}}$ .



# Kinematic invariants

## Theorem

- *The kinematic invariants field is generated by first-order basis differential invariants and by basis invariant derivations. This field separates regular orbits.*
- *For the general cases of  $h(a)$ , as well as for  $h(a) = \lambda_1 a^{\lambda_2}$ ,  $h(a) = \lambda_1 e^{\lambda_2 a}$  and  $h(a) = \ln a$ , the basis differential invariants are*

$$a, \quad u, \quad \rho, \quad s, \quad u_a, \quad \rho_a, \quad s_t, \quad s_a,$$

*and the basis invariant derivations are*

$$\frac{d}{dt}, \quad \frac{d}{da}.$$

# Kinematic invariants

## Theorem

- For the cases  $h(a) = \text{const}$ ,  $h(a) = \lambda a$  and  $h(a) = \lambda a^2$ , the basis differential invariants are

$$\rho, \quad s, \quad u_a, \quad \rho_a, \quad s_a, \quad s_t + u s_a,$$

and basis invariant derivations are

$$\frac{d}{dt} + u \frac{d}{da}, \quad \frac{d}{da}.$$

- The number of independent invariants of pure order  $k$  is equal to 4 for  $k \geq 1$ .

# Euler invariants

Let  $h(a)$  be an arbitrary function.

If the thermodynamic state admits a one-dimensional symmetry algebra generated by the vector field

$$\xi_1 X_2 + \xi_2 X_3 + \xi_3 X_4 + \xi_4 X_5,$$

then the field of Euler differential invariants is generated by the differential invariants

$$a, \quad \left( s - \frac{\xi_2}{\xi_4} \right) \rho, \quad u, \quad u_a, \quad \frac{\rho_a}{\rho}, \quad s_t \rho, \quad s_a \rho$$

of the first order and by the invariant derivations

$$\frac{d}{dt}, \quad \frac{d}{da}.$$

# Euler invariants

Let  $h(a) = \lambda a^2$ ,  $\lambda \neq 0$ .

If the thermodynamic state admits a one-dimensional symmetry algebra generated by the vector field

$$\xi_1 X_2 + \xi_2 X_3 + \xi_3 X_4 + \xi_4 X_5 + \xi_5 X_8 + \xi_6 X_9,$$

then the field of Euler differential invariants is generated by the differential invariants

$$\left( s - \frac{\xi_2}{\xi_4} \right) \frac{\rho_a}{\rho s_a}, \quad u_a, \quad \rho_a \rho^{\frac{\xi_5}{\xi_4 - 2\xi_5} - 1}, \quad \frac{s_a \rho^4}{\rho_a^3}, \quad \frac{(s_t + u s_a) \rho^3}{\rho_a^2}$$

of the first order and by the invariant derivations

$$\frac{d}{dt} + u \frac{d}{da}, \quad \rho^{\frac{\xi_5}{\xi_4 - 2\xi_5}} \frac{d}{da}.$$

## Quotient equation

Our goal is to study a quotient equation for the case:  $h(a) = \lambda a^2$ ,  $\lambda \neq 0$ .

It follows from theorem above that there are four relations (syzygies) between the following second order invariants

$$\frac{du_a}{d\rho}, \quad \frac{d\rho_a}{d\rho}, \quad \frac{dT_a}{d\rho}, \quad \frac{d(T_t + uT_a)}{d\rho},$$
$$\frac{du_a}{dT}, \quad \frac{d\rho_a}{dT}, \quad \frac{dT_a}{dT}, \quad \frac{d(T_t + uT_a)}{dT},$$

where

$$\frac{d}{d\rho} = \frac{1}{\rho_t T_a - \rho_a T_t} \left( T_a \frac{d}{dt} - T_t \frac{d}{da} \right),$$
$$\frac{d}{dT} = \frac{1}{\rho_t T_a - \rho_a T_t} \left( -\rho_a \frac{d}{dt} + \rho_t \frac{d}{da} \right)$$

are Tresse derivatives.

## Quotient equation

Choosing  $\rho$  and  $T$  as Lie–Tresse coordinates  $(x, y)$  and  $K(x, y) = u_a$ ,  $L(x, y) = \rho_a$ ,  $M(x, y) = T_a$ ,  $N(x, y) = T_t + uT_a$  as unknown functions, respectively, if  $u^2 + p_x \neq 0$ ,  $xKM + LN \neq 0$ ,  $M \neq 0$ , we get the quotient equation  $E_q$

$$\left\{ \begin{array}{l} xKM_x - NM_y + LN_x + M(N_y - K) = 0, \\ k(LM_x + MM_y) + xy(xKs_x - Ns_y) = 0, \\ L(x(p_{xx}L^2 + 2p_{xy}LM + p_{yy}M^2) + \\ (xLL_x + xML_y - L^2)p_x + (xLM_x + xMM_y - LM)p_y) + \\ x^2(KNL_y - xK^2L_x + (xKM + LN)K_y + 3LK^2 + \omega^2L) = 0, \\ M(x(p_{xx}L^2 + 2p_{xy}LM + p_{yy}M^2) + \\ (xLL_x + xML_y - L^2)p_x + (xLM_x + xMM_y - LM)p_y) - \\ x(N^2L_y - xKNL_x + (xKM + LN)xK_x + 2LKN - xM(K^2 + \omega^2)) = 0. \end{array} \right.$$

## Quotient equation

The symbol of the quotient equation  $E_q$  is

$$\begin{pmatrix} 0 & 0 & k(L\xi_1 + M\xi_2) & 0 \\ 0 & 0 & xK\xi_1 - N\xi_2 & L\xi_1 + M\xi_2 \\ x^2(xKM + LN)\xi_2 & A & xp_y L(L\xi_1 + M\xi_2) & 0 \\ -x^2(xKM + LN)\xi_1 & B & xp_y M(L\xi_1 + M\xi_2) & 0 \end{pmatrix},$$

where

$$A = x(p_x L^2 - x^2 K^2)\xi_1 + x(p_x LM + xKN)\xi_2,$$

$$B = x(p_x LM + xKN)\xi_1 + x(p_x M^2 - N^2)\xi_2.$$

Its determinant has the form

$$kx^3(xKM + LN)(L\xi_1 + M\xi_2)^2 ((L\xi_1 + M\xi_2)^2 p_x - (xK\xi_1 - N\xi_2)^2),$$

which gives us three characteristic vector fields of  $E_q$ :

$$Z_1 = L\partial_x + M\partial_y, \quad Z_{2,3} = xK\partial_x - N\partial_y \pm \sqrt{p_x}(L\partial_x + M\partial_y).$$

## Quotient equation

We find solution of the quotient for the case of ideal gas. Recall that the thermodynamic state is given by the Planck potential  $\Phi(x, y)$ , which for the case of ideal gas is the following

$$\Phi(x, y) = \frac{n}{2} \ln y - \ln x,$$

where  $n$  is a number of freedom degrees of a gas particle. Pressure and entropy are expressed in terms of  $\Phi(x, y)$ :

$$p(x, y) = -Rx^2 T \Phi_x, \quad s(x, y) = R(\Phi + y \Phi_y),$$

where  $R$  is a specific gas constant.

Moreover, we consider solutions of the quotient equation  $E_q$  that are constant along the field  $Z_1$ .



## Quotient equation

Let us require the functions  $M$  and  $L$  be the first integrals of the vector field  $Z_1$ . Then solving an overdetermined system  $E_q \cup \{Z_1(L) = Z_1(M) = 0\}$ , we obtain the following of solutions of the quotient  $E_q$ :

$$L = 0, \quad M = c_1 x^{1+\frac{2}{n}}, \quad K = \sqrt{c_2 x^2 - \omega^2}, \quad N = -\frac{2y \sqrt{c_2 x^2 - \omega^2}}{n},$$

$$L = c_1 \left(\frac{x}{y}\right)^{\frac{2n}{n-2}}, \quad M = \frac{y}{x} L, \quad K = \sqrt{c_2 \left(\frac{x}{y}\right)^{\frac{2n}{n-2}} - \omega^2}, \quad N = -\frac{2Ky}{n},$$

where  $c_1 \neq 0$ ,  $c_2$  are constants.

## Euler solutions

Now we use the first solution of  $E_q$  to solve the Euler system. Recalling that  $x, y, K, L, M, N$  are invariants and adding their expressions to the Euler system, we get a finite-type system

$$\left\{ \begin{array}{l} \rho_a = 0, \quad T_a = c_1 \rho^{1+\frac{2}{n}}, \quad u_a = \sqrt{c_2 \rho^2 - \omega^2}, \\ T_t + u T_a = -\frac{2T}{n} \sqrt{c_2 \rho^2 - \omega^2}, \\ \rho(u_t + uu_a) + R\rho T_a + \omega^2 \rho_a = 0, \\ \rho_t + \rho u_a = 0, \\ 2kT_{aa} - Rn\rho(T_t + uT_a) + 2RT\rho_t = 0. \end{array} \right.$$

This system is overdetermined, and solving it, we get expressions for the pressure, density, temperature and velocity.

# Euler solutions

$$\rho = \frac{\omega}{\sqrt{c_2} \cos(c_3 - \omega t)}, \quad u = a\omega \tan(c_3 - \omega t) + f(t),$$

$$T = c_1 a \rho^{1 + \frac{2}{n}} \cos^{-\frac{2}{n}}(c_3 - \omega t) \left( c_1 c_2^{-\frac{n+2}{2n}} \omega^{\frac{n+2}{n}} \int \frac{f(t)}{\cos(c_3 - \omega t)} dt + c_5 \right),$$

where

$$f(t) = \frac{-R c_1 c_2^{-\frac{n+2}{2n}} \omega^{\frac{n+2}{n}}}{\cos(c_3 - \omega t)} \left( \int \cos^{-\frac{2}{n}}(c_3 - \omega t) dt + c_4 \right)$$

and  $c_1 \neq 0, c_2 > 0, \dots, c_5$  are constants.

## Euler solutions

Doing the same with the second solution of the quotient:

$$L = c_1 \left( \frac{x}{y} \right)^{\frac{2n}{n-2}}, \quad M = \frac{y}{x} L, \quad K = \sqrt{\frac{c_2}{c_1} L - \omega^2}, \quad N = \frac{-2Ky}{n},$$

we have

$$u = a\omega \tan(c_3 - \omega t) + 2f(t), \quad T = \rho \left( \frac{c_2 \cos^2(c_3 - \omega t)}{\omega^2} \right)^{\frac{n-2}{2n}},$$

$$\rho = \frac{c_1 \omega^2 a}{c_2 \cos^2(c_3 - \omega t)} - \frac{c_1 \omega^2}{c_2 \cos(c_3 - \omega t)} \left( \int \frac{2f(t)}{\cos(c_3 - \omega t)} dt + c_5 \right),$$

where  $f(t)$  is the same as before, and  $c_1, \dots, c_5$  are constants.

# Literature



V. Lychagin, *Contact Geometry, Measurement and Thermodynamics*, in: *Nonlinear PDEs, Their Geometry and Applications. Proceedings of the Wisla 18 Summer School*, Springer Nature, Switzerland, 3-54 (2019).

Thank you for attention.